



Opportunities for Research in Energy and Power Electronics at Monash University

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In association with
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with thanks to
Centre for Power Electronic Systems, Virginia Tech

Introduction



- Electrical Power at Monash University a short walk through history
- What is this business called Power Electronics ?
- Power Electronics research activities at Monash
- Other Electrical Power Research Activities
 - The EPRI Project
 - High Voltage
 - Renewable Energy
- Summary



- Electrical Power has been a part of Monash Electrical Engineering since department was established.
- It has been a major contributor to both Teaching and Research.
- The focus of activities has changed over the years as older technologies have matured and new technologies have developed.
- One thing remains certain electrical power is an essential service on which we all depend.



- From 1960's to 1980's, electrical power generation, transmission and reticulation blossomed in South East Australia
- Transmission System voltages jumped from 132 kV to 220 kV to 500 kV
- Generator sizes increased from 10's MW to 500 MW units
- Many innovative ideas were implemented (SWER, SCADA control)
- Research and development in Electrical Power was a major growth activity.



- The major engineering institutions were SECV and ECNSW
- Major research institutions were at Monash, Sydney, and Newcastle
- The background research into the 500 kV transmission system in Victoria was done at Monash
- Major contributions to power system stability were made by Monash during the 1970's



In the 1980's, the focus changed:

- Power systems research moved to consider economic issues as well as technical matters
- New types of plant appeared, using power electronic conversion systems
- Monash incorporated Power Electronics into its Electrical Power research and teaching
- Electrical Power became "mature" in the community, always available, always reliable



In the 1990's there were huge changes in the electrical power supply industry

- State owned utilities were broken up into small competing private companies, in the name of "efficiency"
- Economics became the dominant concern
- Companies focused on "what they were good at" – selling electricity, serving customers
- Central planning effectively ceased, leaving "the market to provide"
- The changes are in still progress!



Electrical Power at Monash has managed to weather this storm for over a decade (well, at least we are still here!)

- The Centre for Electrical Power Engineering was established in 1991 as a final contribution from the SECV
- 8 academics were employed for over 5 years
- Research activities developed in several areas
- Power Electronics established itself as a major international research contributor



Unfortunately nothing lasts forever!

- Funding from the electrical power generation industry has been greatly reduced
- The focus of the industry is on training and management of the existing resources, not new developments
- Electrical Power and Energy at Monash must find a new focus if it is to continue
- Power Electronics and Industrial Electronics is a world wide R&D growth market, so that is becoming a major new focus for Monash.

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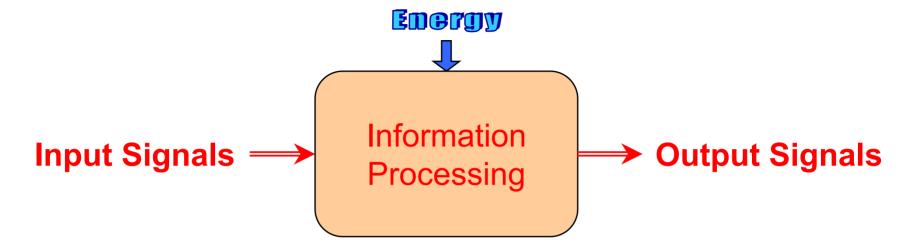
- Power: turns the lights on
- Electronics: transistor radios

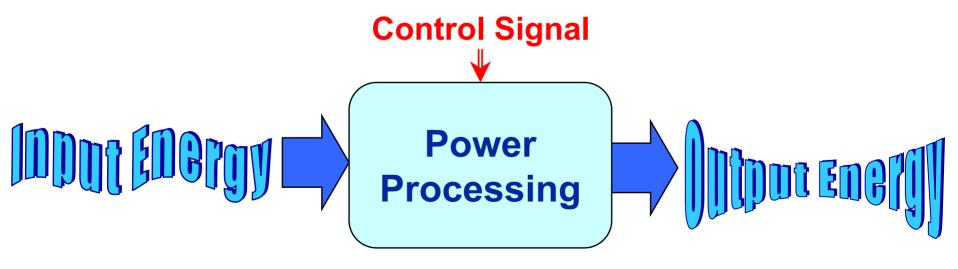
But what is Power Electronics?

- Power Electronic Systems use electronics to control Electrical Energy usage
- Power levels range from milliwatts to megawatts
- The common element is a switched energy conversion process, smoothed by input and output filters



Microelectronics vs. Power Electronics



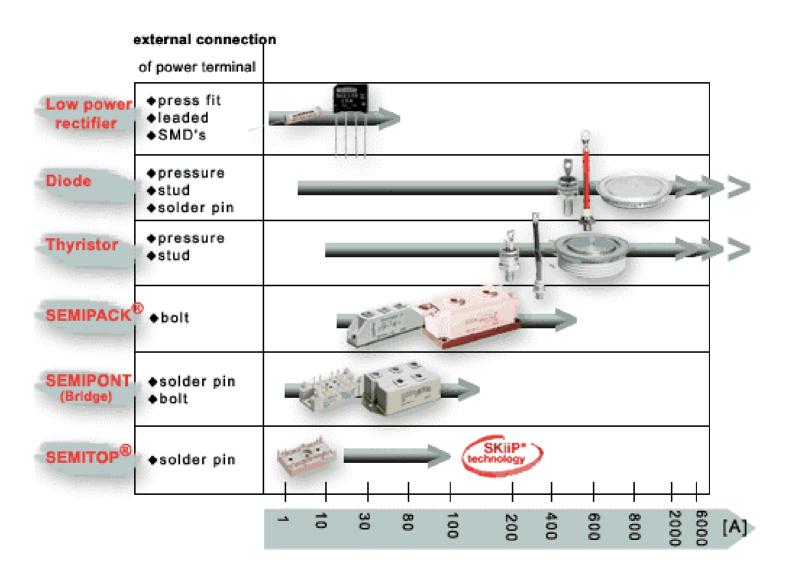




- Power Electronic converters have existed for nearly 40 years.
- Initially based on Silicon Controlled Rectifiers (controlled turn-on, uncontrolled turn-off).
- Modern semiconductor devices are:
 - Power MosFET's, 100's volts, 10's amps
 - Insulated Gate Bipolar Transistors (IGBT), 2000+ volts, 500 A
 - Insulated Gate Controlled Thyristor (IGCT), 4000+ volts, 1000's amps.
 - Gate Turn Off Thyristor (GTO), 6000+volts, 1000's amps

Electrical Power Engineering

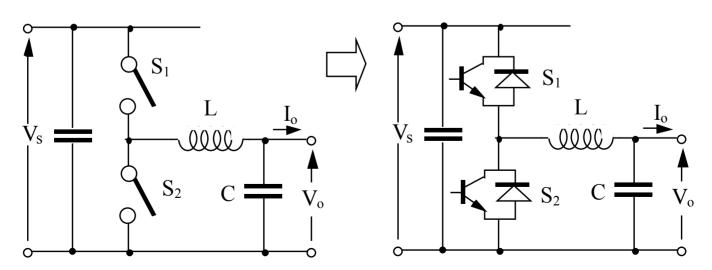




Courtesy: Semikron website

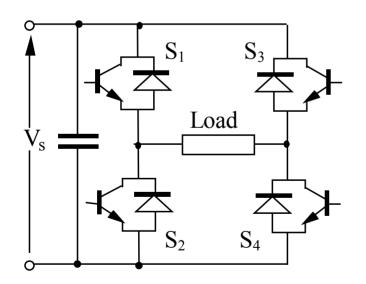


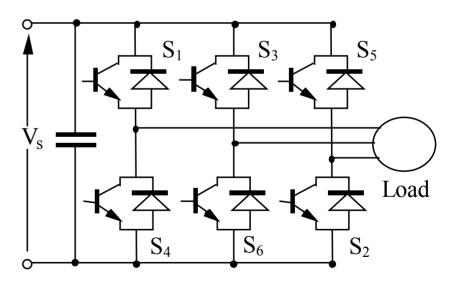
- Basic cell structure is half bridge phase leg
- Generic form uses ideal switches that can block block <u>bi</u>-directional volt, conduct <u>bi</u>-directional current
- Conventional form uses transistor/diode combination that can block <u>uni</u>-directional volt
- Input is voltage stiff, Output is current stiff, transfer function is stepdown (buck).





- Voltage Source Inverter (VSI)
 - Smooth DC Input Voltage, Switched Input Current
 - Switched AC Output Voltage, Smooth Output Current
 - Bi-directional current and power flow
 - > Step down voltage transfer ratio

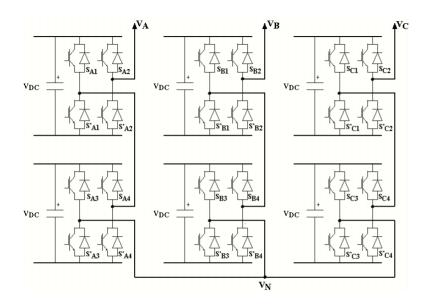


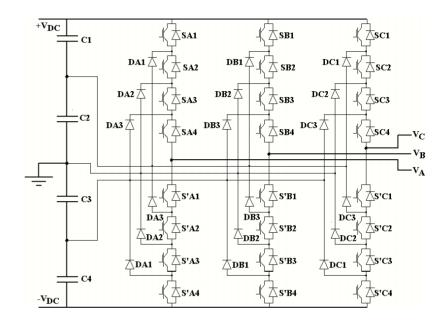


Single Phase

Three Phase







Cascaded Topology

- Isolated DC Supplies
- Suitable for High Num Levels
- Hybrid Unequal Supplies

Diode Clamped Topology

- One DC bus
- Capacitors form Levels
- Voltage Balance restricts
 No. Levels



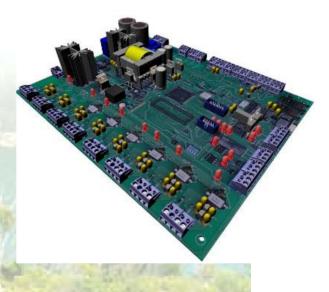
- Open Loop Modulation is the processing of controlling the actual switching of the semiconductor elements
- Closed Loop Regulation is a feedback arrangement to control the modulation to achieve a controlled variable outcome
- Applications are combinations of modulation and regulation processes operating as complete working systems
- Analogue controlled systems are common historically and still used for simple applications
- Digitally controlled systems are much more common and essentially now dominate



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- Power Electronics Group (PEG) at Monash was started in 1995
- Staff comprises:
 - 2 academic faculty
 - employed research engineers
 - post-graduate students Masters and PhD.
- PEG undertakes both fundamental research and practical commercial developments
- Research activities include:
 - PWM modulation
 - Open and Closed Loop control of VSI/CSI
 - Active Filters & other Custom Power applications
 - Distributed Generation in weak grid systems
 - Traction systems





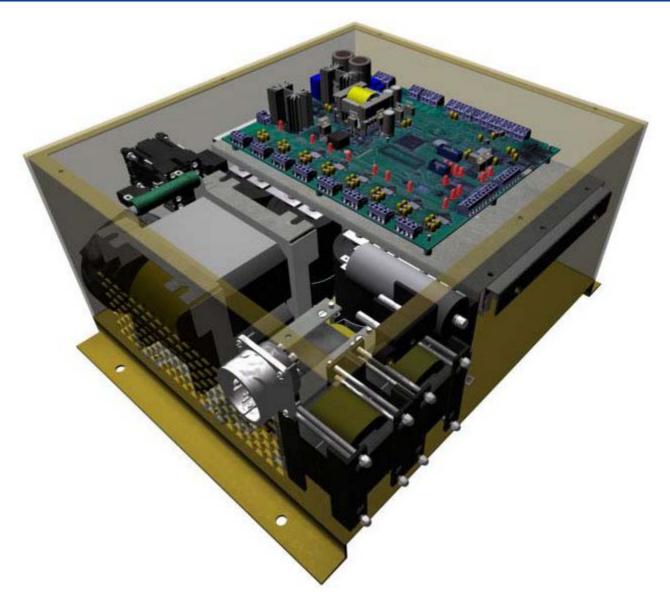
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<u>Advances in Modulation Theory</u>

1970's: Major steps forward

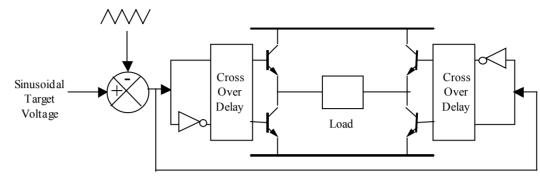
1980's: Minor improvements

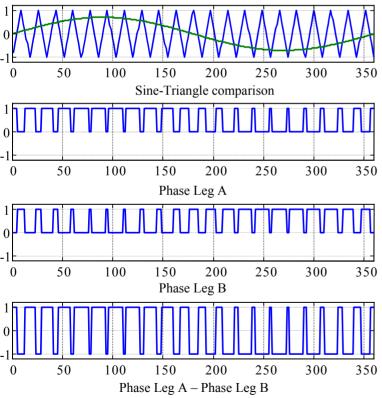
Since then - refinements, despite many hundreds of papers !!!

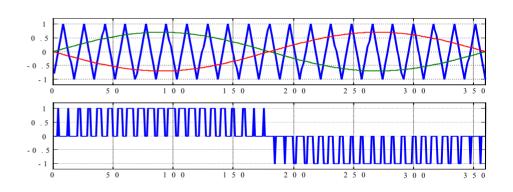
Finally, consolidation has been achieved in the last few years, with significant contributions from PEG



Simplest strategy is sin-triangle PWM







THREE LEVEL PWM

TWO LEVEL PWM

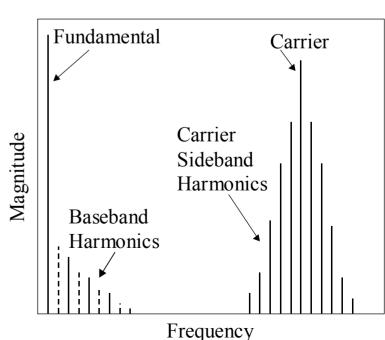
Analytical Solution is obtained by Double Fourier Analysis of the Switched Phase Leg Output Waveform, which gives:

$$F(t) = \frac{A_{00}}{2} + \sum_{n=1}^{\infty} \begin{cases} A_{0n} \cos(n\omega_o t) + \\ B_{0n} \sin(n\omega_o t) \end{cases} + \sum_{m=1}^{\infty} \begin{cases} A_{m0} \cos(m\omega_c t) + \\ B_{m0} \sin(m\omega_c t) \end{cases} + \sum_{m=1}^{\infty} \sum_{\substack{n=-\infty \\ n\neq 0}}^{\infty} \begin{cases} A_{mn} \cos(m\omega_c t + n\omega_o t) + \\ B_{mn} \sin(m\omega_c t + n\omega_o t) \end{cases}$$

$$C_{mn} = A_{mn} + jB_{mn} = \frac{1}{2\pi^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} F(x, y) e^{j(mx+ny)} dxdy$$
, $x = \omega_c t, y = \omega_o t$

The solution contains:

- Fundamental component
- Baseband Harmonics
- Carrier Harmonics
- Sideband Harmonics

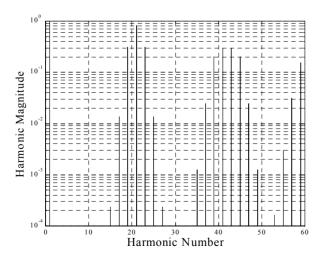




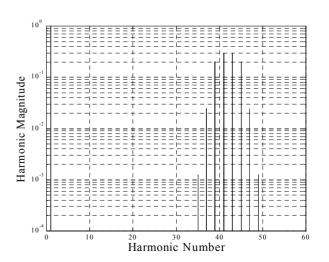
Analytical Solution for one Phase Leg is

$$\begin{split} v_{an}(t) &= V_{dc} + MV_{dc}\cos(\omega_{o}t + \theta_{o}) + \sum_{m=1}^{\infty} \left[\frac{4V_{dc}}{m\pi} J_{0} \left(m\frac{\pi}{2}M \right) \sin m\frac{\pi}{2}\cos(m[\omega_{c}t + \theta_{c}]) \right] \\ &+ \sum_{m=1}^{\infty} \sum_{\substack{n=-\infty\\(n\neq 0)}}^{\infty} \frac{4V_{dc}}{m\pi} J_{n} \left(m\frac{\pi}{2}M \right) \sin\left([m+n]\frac{\pi}{2} \right) \cos\left(m[\omega_{c}t + \theta_{c}] + n[\omega_{o}t + \theta_{o}] \right) \end{split}$$

Harmonics cancel between phase legs differently for two level and three level modulation



Two level PWM

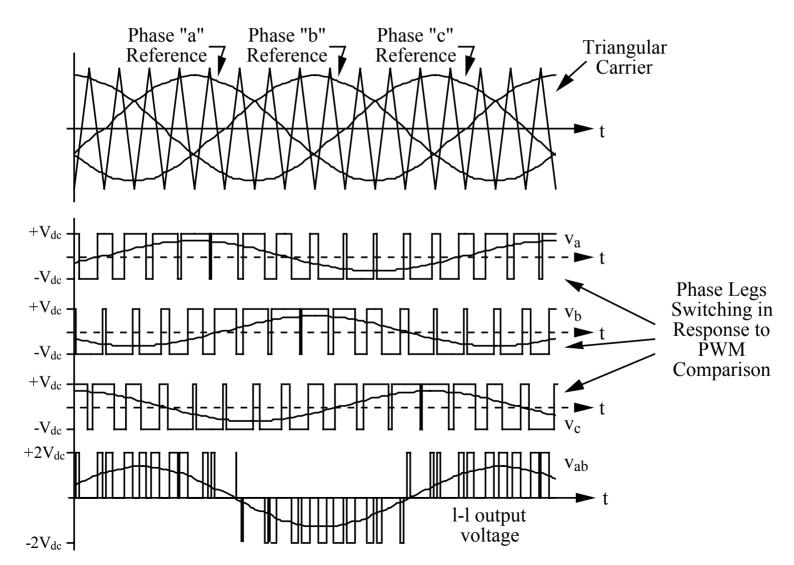


Three Level PWM

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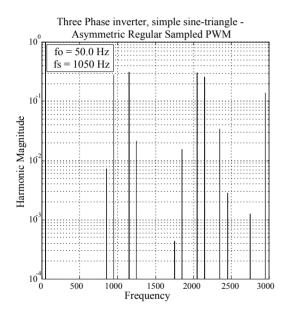


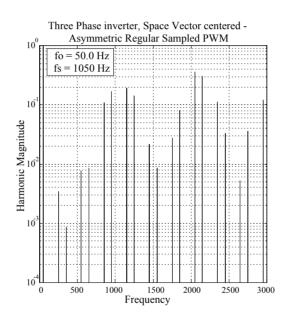
Three phase inverters use the same strategy with reference waveforms that are displaced in time by 120°.

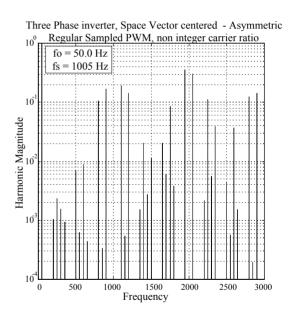




Now the harmonics cancel between the phase legs differently, since the reference offset angles are different.







Simple Sine References

Third Harmonic Reference

Asynchronous Pulse Ratio

 ΔT

 t_{i-1}

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 SV_{\min}

 \overline{SV}_1

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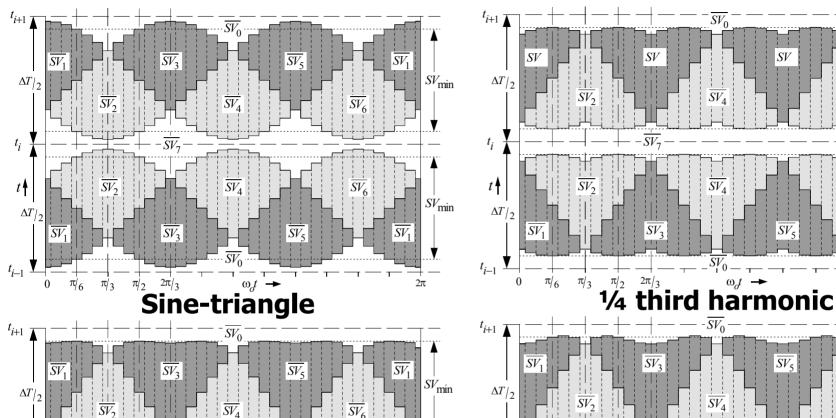
 $\overline{SV_6}$

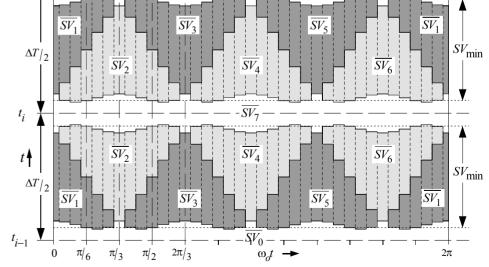
SV



 SV_{\min}

 SV_{\min}

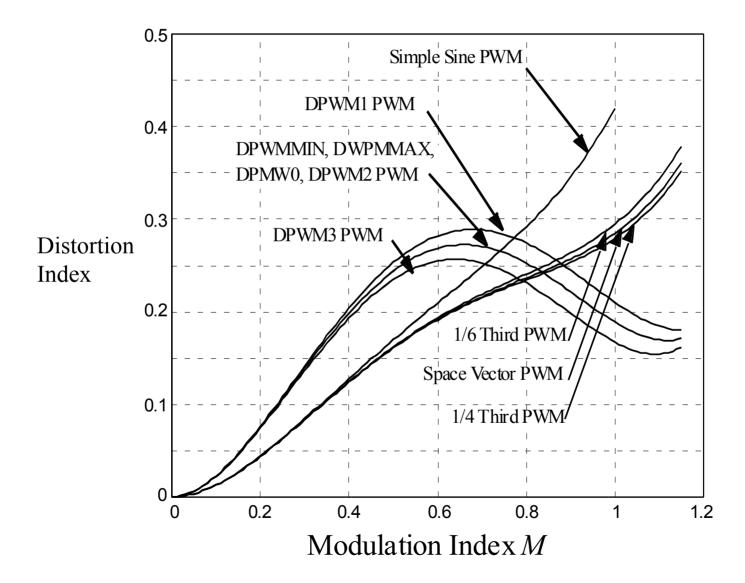




1/6 third harmonic

Space vector





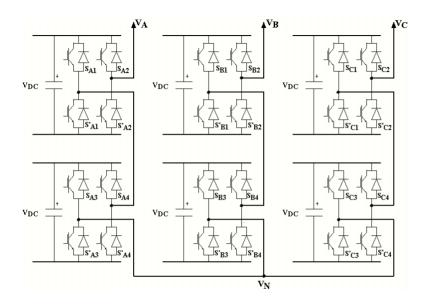


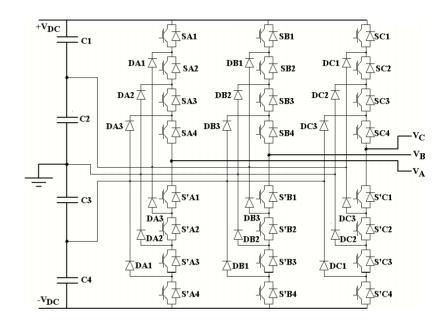


PWM applied to Multilevel converters

- POD/APOD/PD Sine-triangle modulation strategies
- Equivalence of Sine-triangle and SV modulation
- Reduced common mode PWM strategies







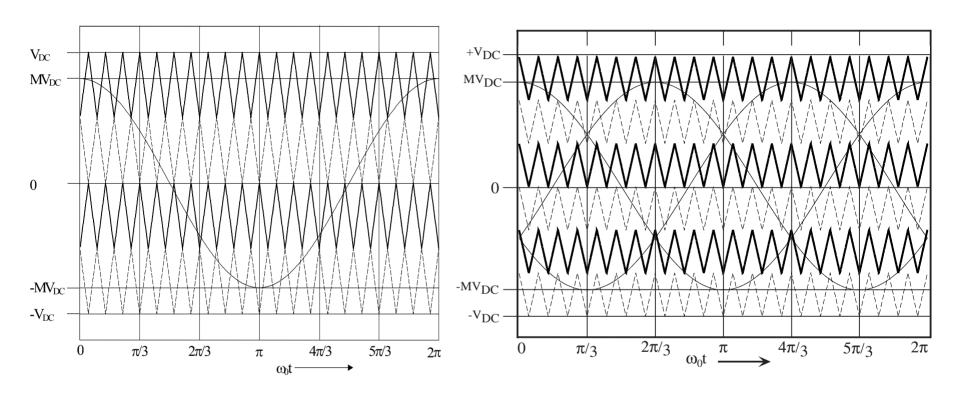
Cascaded Topology

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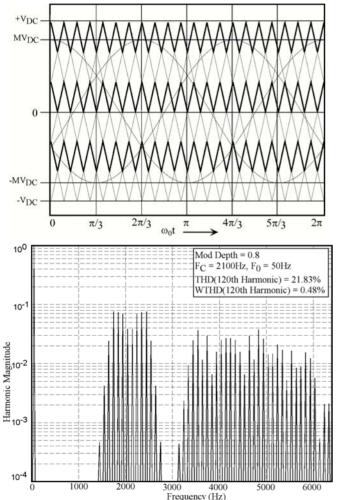
5 Level APOD Modulation

5 Level PD Modulation

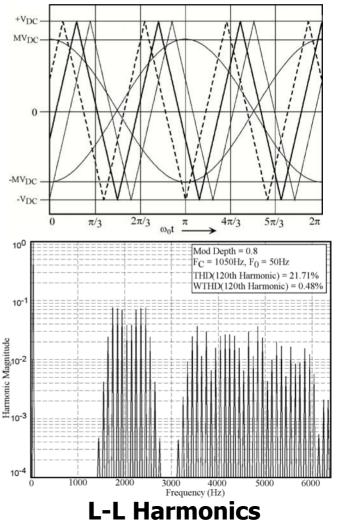
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Multilevel PWM is more complex to develop analytical solutions. However, the results identify a direct match between NPC APOD and cascaded inverter modulation.

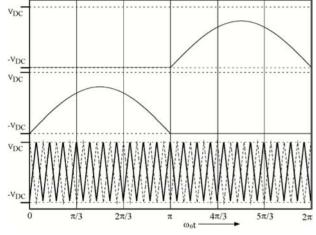


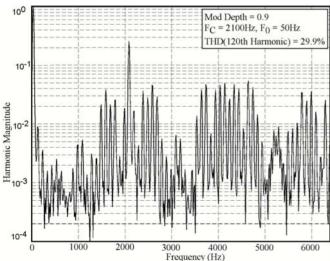
Phase Leg Harmonics

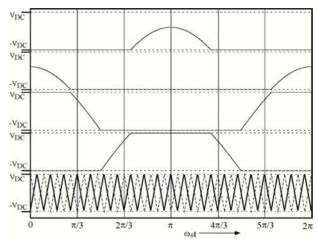


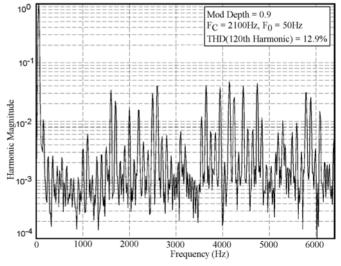


This in turn allows a new modulation strategy to be developed for Cascaded Inverters, which achieves PD type harmonic response.











- Target Objectives of a modulation system are to switch an inverter to achieve an "average" output voltage.
- Once this is achieved, the secondary objectives of reduced harmonics and minimised losses can be considered.
- These objectives are achieved by using the three nearest active space vectors to the target reference phasor, and placing these vectors centrally in the carrier period.
- Carrier-based and SV strategies can achieve identical harmonic results provided a suitable offset waveform is defined.
- Concepts readily extrapolate to multilevel inverters.

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An integrated and comprehensive theory of PWM

The selection of the best algorithm for optimum pulse width modulation is an important process that can result in improved converter efficiency, better load (motor) efficiency, and reduced electromagnetic interference. However, the identification of the best approach is a complex process requiring extensive mathematical manipulation.

Pulse Width Modulation for Power Connectors: Principles and Practice is the first single-volume resource written to help researchers in the field attain a working knowledge of the subject. The authors bring together today's seemingly diverse approaches into a single integrated and comprehensive theory of modulation.

The book provides a generalized approach to the fundamentals of PWM, looking at:

- · active switch pulse width determination
- active switch pulse placement within a switching period
- active switch pulse requence between phase legs and across switching periods

The benefits of this generalized concept is that once the common threads are identified, the selection of a modulation strategy for any conventer topology becomes immediately clear, leaving only secondary factors, such as practical performance, cost and difficulty of implementation, to consider. Additionally, it allows the performance of any periturbar converter topology and PWM strategy to be quickly and easily identified without complex and time-consuming analysis. Patre Within Mechalistics for Power Converters. Proceepins and Practices enables the reader to achieve optimum PWM results for any application.

 D. GRAHAME HOLMES is a professor in the Department of Electrical and Computer Systems Engineering at Monash University in Australia.

THOMAS A. LIPO is a professor the Department of Electrical and Computer Engineering at the University of Wisconsin-Madison, USA.



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PULSE WIDTH MODULATION FOR POWER CONVERTERS

Holmes Lipo



Pulse Width Modulation For Power Converters

PRINCIPLES AND PRACTICE

D. Grahame Holmes Thomas A. Lipo

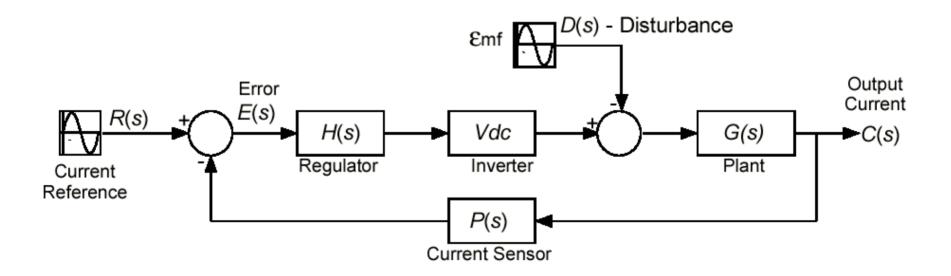
Mohamma E. El-Harrary, Junior Editor

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\begin{split} & \frac{A_{ij}}{A_{ij}} + \sum_{g \in \mathcal{G}} \left( a_{ij} \left( a_{ij} + \theta_{g} \right) + B_{gin} \sin \left( a_{ij} \left( a_{ij} + \theta_{g} \right) \right) \right) \\ & \text{Recommend Correspondents} \\ & + \sum_{g \in \mathcal{G}} \left[ A_{ij} \cos \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) + B_{ij0} \sin \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) \right] \\ & = 1 \\ & + \sum_{g \in \mathcal{G}} \left[ A_{ij0} \cos \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) + B_{ij0} \sin \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) \right] \\ & + \sum_{g \in \mathcal{G}} \left[ A_{ij0} \cos \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) + B_{ij0} \sin \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) \right] \\ & + B_{ij0} \sin \left( m \left[ \alpha_{g} t + \theta_{g} \right] + B_{ij0} \sin \left( m \left[ \alpha_{g} t + \theta_{g} \right] \right) \right] \end{split}
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LINEAR CLOSED LOOP CONTROL

- Conventional Closed Loop Control uses
 Proportional and integral Gain in the forward path to minimise error.
- Typical application is current controlled inverter



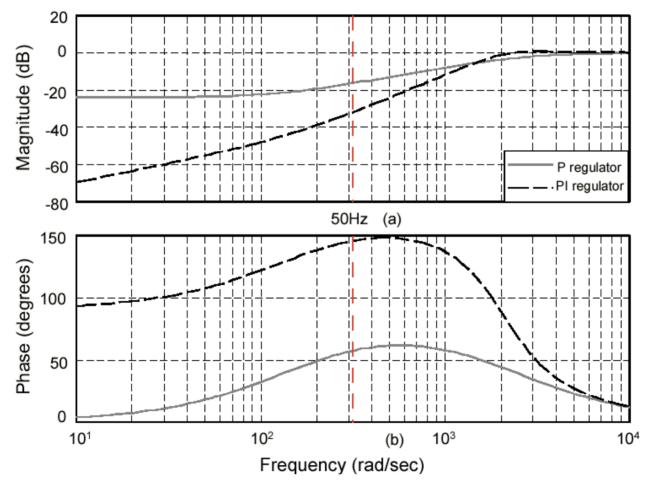
Power

Group

Electronics



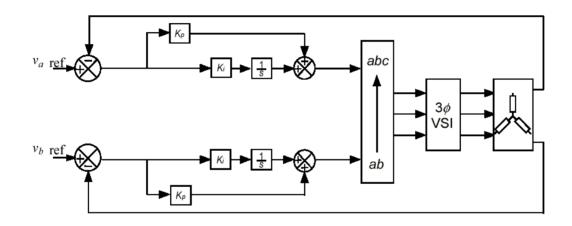
This type of system is known to create steady state error for AC regulation systems.

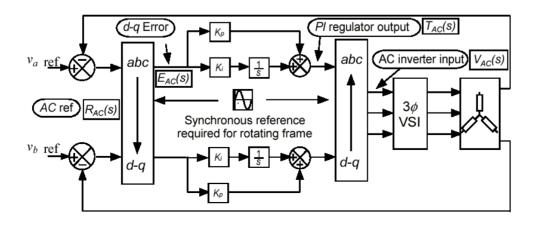


Plot of error verses reference as frequency varies



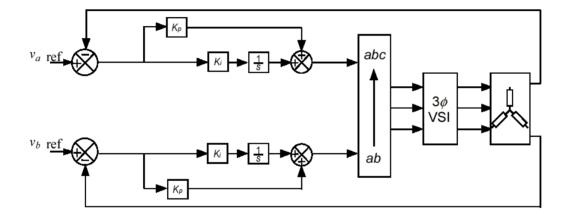
- For Three Phase systems, regulation in the synchronous d-q frame eliminates steady state error.
- There is no simple single phase equivalent

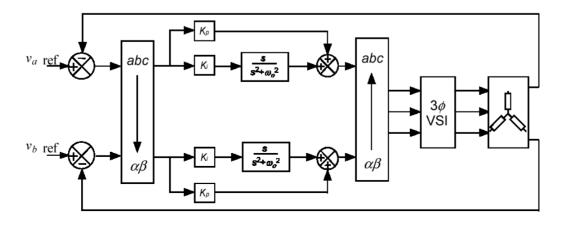






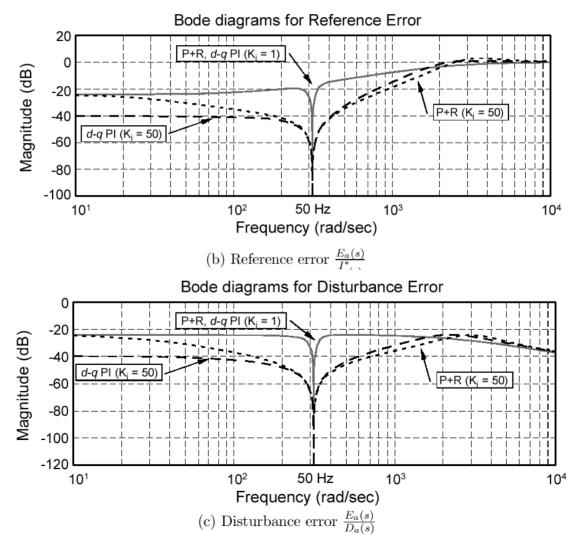
- Can get an equivalent response by implementing a resonant gain block in the stationary frame.
- Equally applicable to single or three phase systems





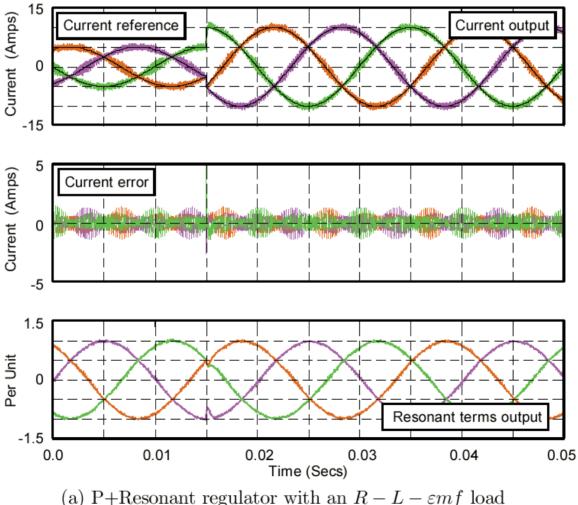


 The notch filter achieved almost infinite gain at the target frequency and hence almost zero error





The performance of the <u>P+ resonant</u> controller is excellent as a current regulator

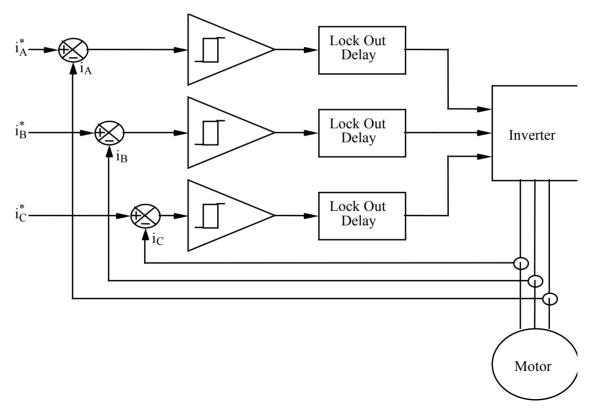


(a) P+Resonant regulator with an $R-L-\varepsilon mf$ load



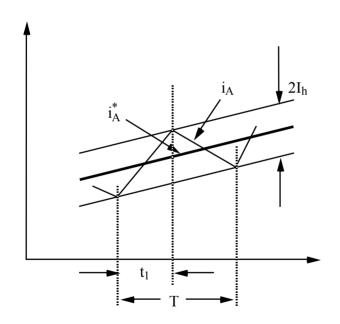
NON LINEAR CONTROL

- Non Linear Converter control systems directly control the switches from the control algorithm.
- Most common example is hysteresis control.





- Non Linear Converter control systems directly control the switches from the control algorithm.
- Most common example is hysteresis control.

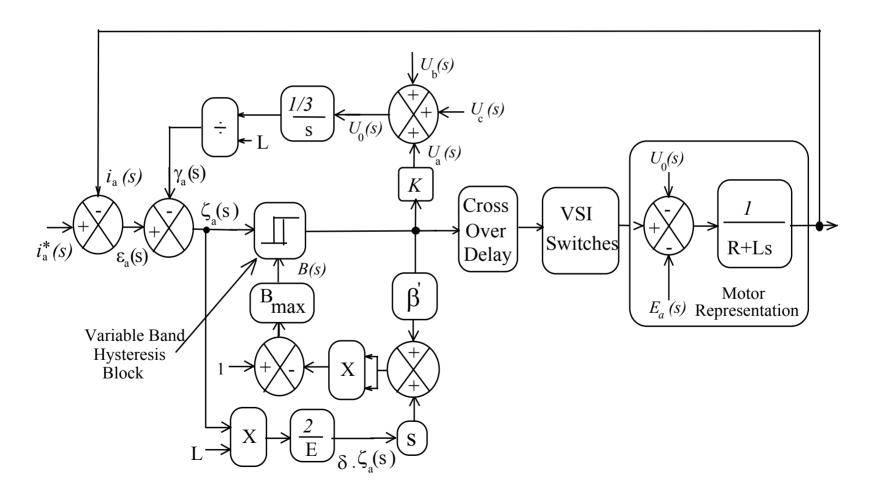


Problems with conventional hysteresis control are:

- Variable frequency switching.
- Sub optimal switching pattern for both single and three phase.
- Limit cycle hazard.



 Variable band width switching solves most of these problems.



0.002

0.004

0.006

0.008

0.01

Time (Secs)

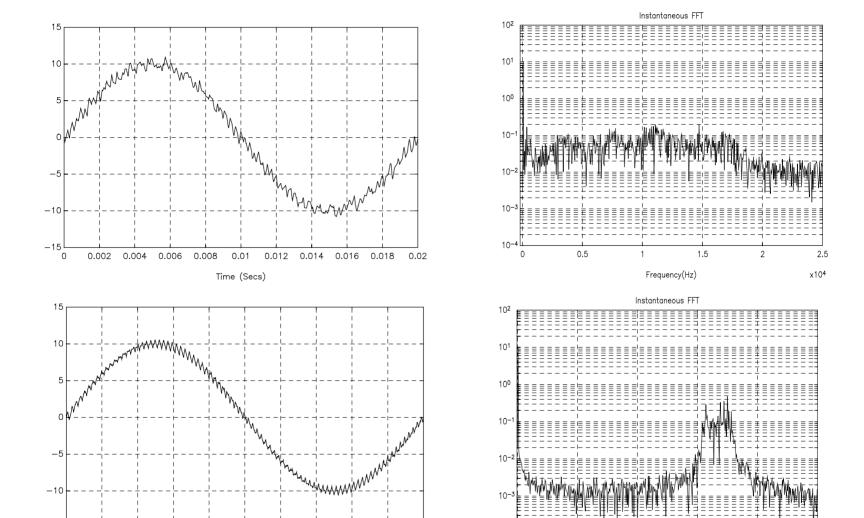
0.012

0.014

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Variable band hysteresis control

0.016

0.018

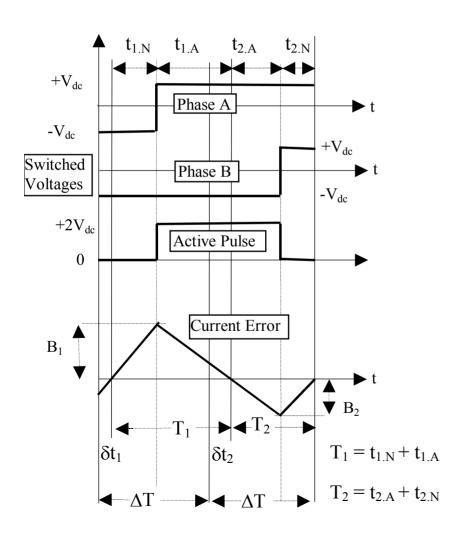
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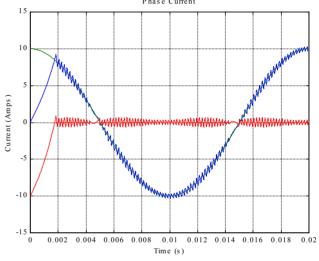
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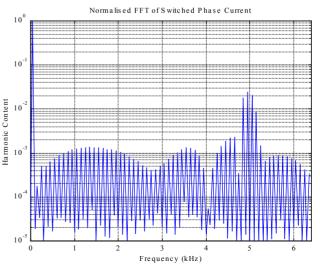
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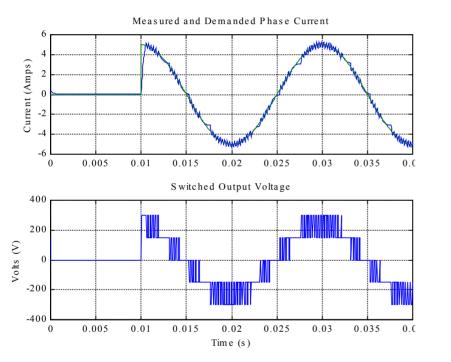
Linking variable band hysteresis with deadbeat control improves the performance even further.

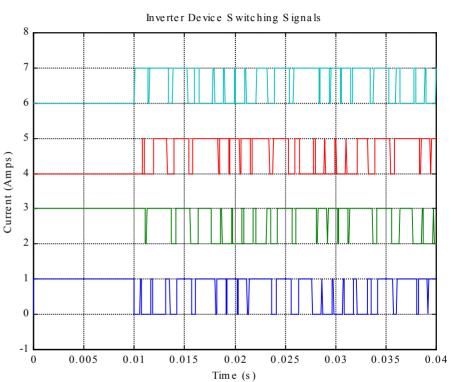












Multilevel Hysteresis Control: 5 Level Cascaded Inverter



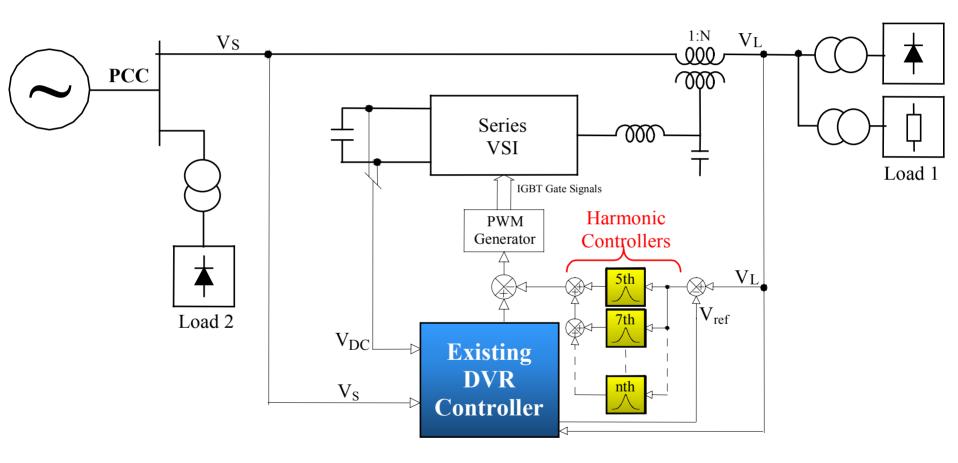
Extending the Power Quality Compensation Capabilities of Dynamic Voltage Restorers

Michael John Newman

Monash University Melbourne, Australia



Proposed additional control system





- DVR primary value adding objective:
 - Sag Compensation
- Other possible value adding objectives:
 - Harmonic voltage compensation



- Harmonic isolation
- Fundamental Voltage Regulation
 - Reactive Injection (requires large series rating fine for DVR)
 - Real Injection (requires power source possibly bi-directional)
- Flicker compensation (more temporary energy storage may be required)
- Swell regulation (requires bi-directional supply)
- Ideal design criteria for value adding DVR systems
 - Addition should not affect the transient response of the DVR
 - The topology should preferably not be altered
 - Primary aim is to provide extra value added services to the customer using the exact same equipment, with minimal adverse affects

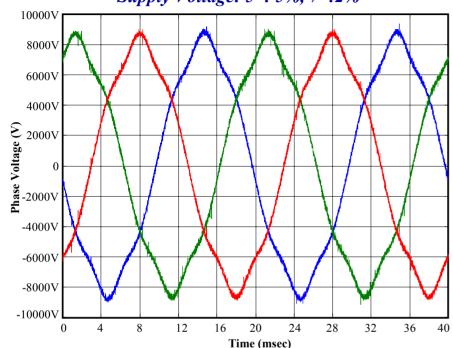








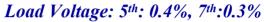


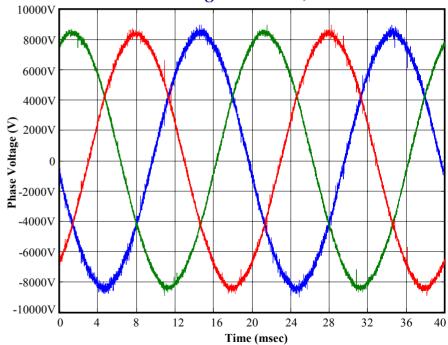


Test 1 Conditions:

- Test AC Voltage: 10kV l-l rms
- Distorted voltage from programmable supply
- Linear passive load (approx. 2kW)
- DC Bus voltage of 400V

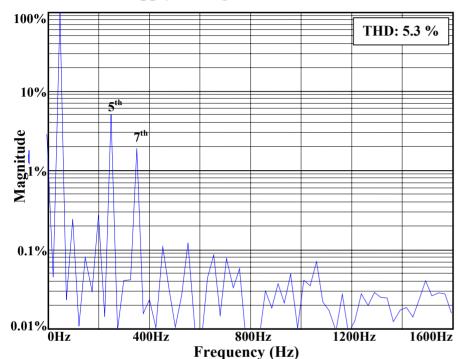
1. Steady-state Results: Distorted Supply







Supply Voltage: 5th: 5%, 7th: 2%

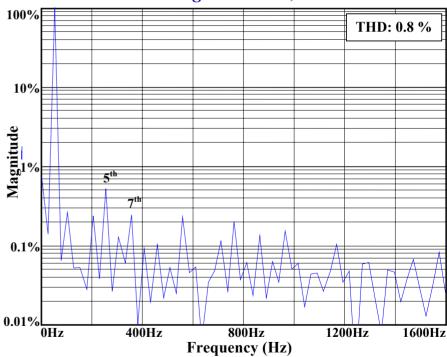


Test 1 Conditions:

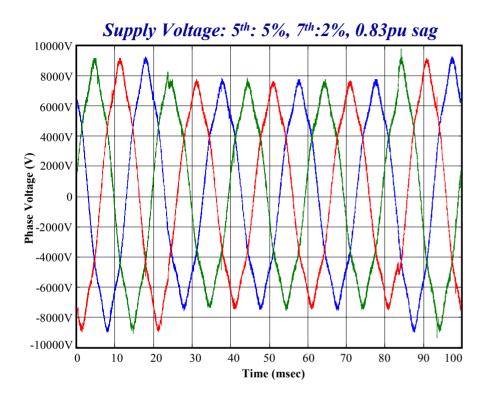
- Test AC Voltage: 10kV l-l rms
- Distorted voltage from programmable supply
- Linear passive load (approx. 2kW)
- DC Bus voltage of 400V

1. Steady-state Results: Distorted Supply

Load Voltage: 5th: 0.5%, 7th:0.25%



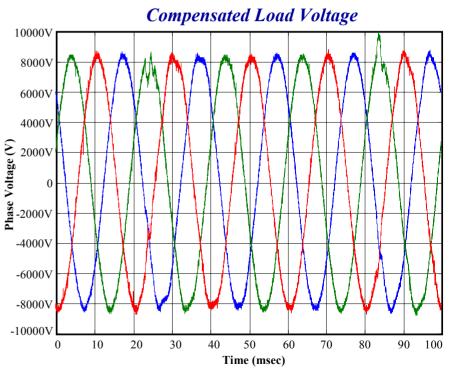




Test 2 Conditions:

- Distorted voltage from programmable supply
- Linear passive load (approx. 2kW)
- 0.83p.u. Sag
- DC Bus voltage of 400V

2. Transient Results: Distorted Supply with Sag





A Robust Multilevel Hybrid Compensation System for 25kV Electrified Railway Applications

P. C. Tan, P. C. Loh, D. G. Holmes

Centre of Electrical Power Engineering,

Dept. of Electrical and Computer System Engineering,

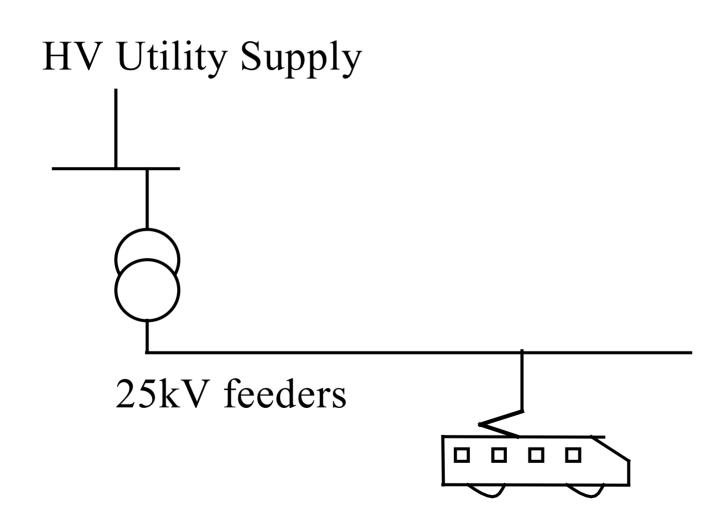
Monash University, Australia





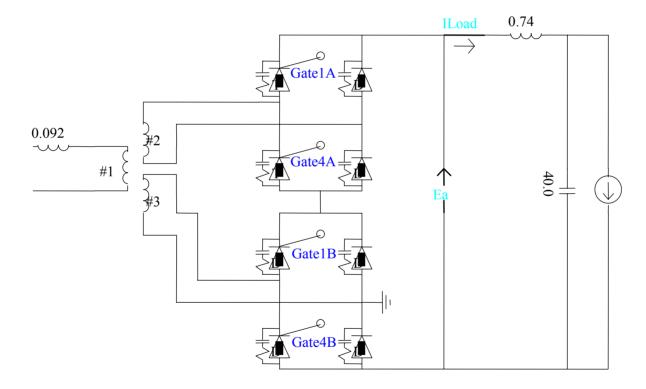


AC Traction System





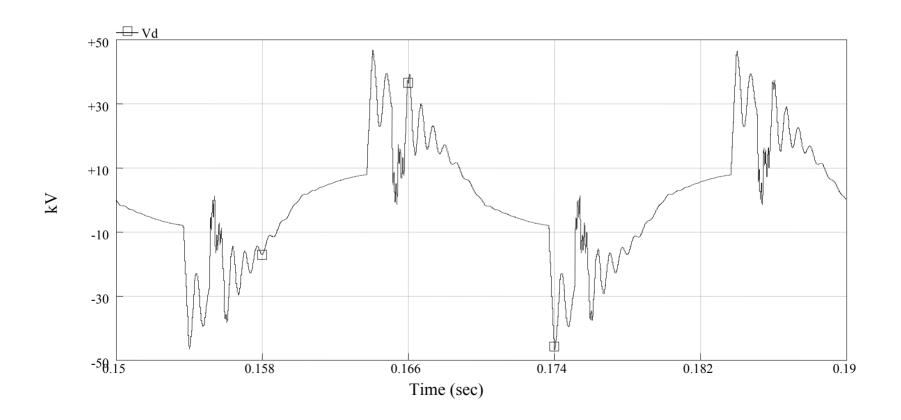
Railway locomotive model





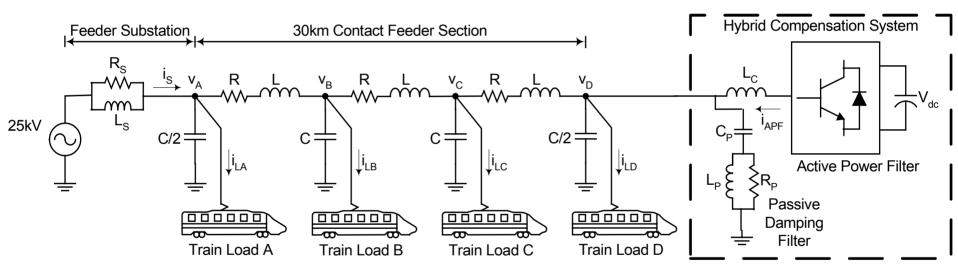


Typical trackside voltage waveform



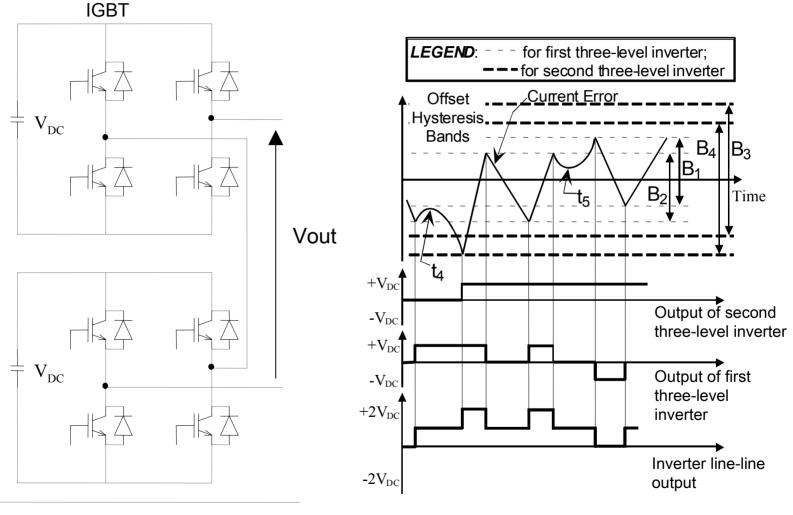


Railway traction system model





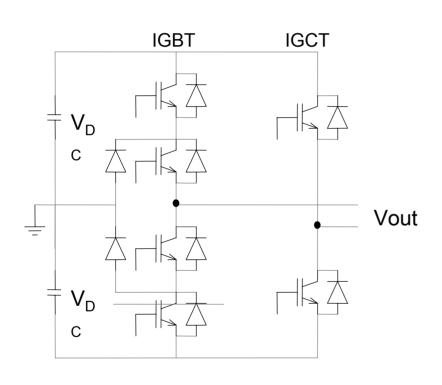
Hysteresis current regulation



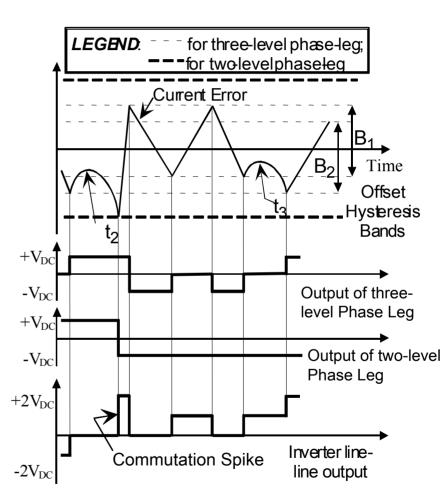
Cascaded inverter



Hysteresis current regulation

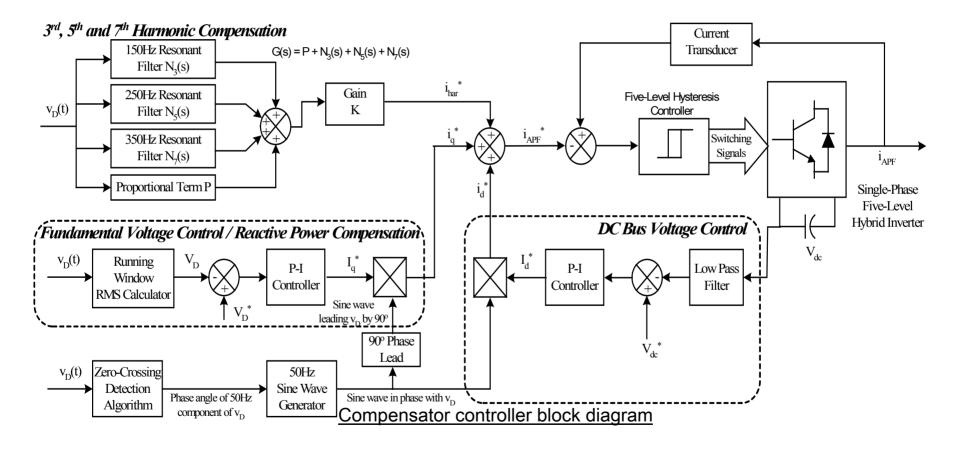


5 level Reduced inverter



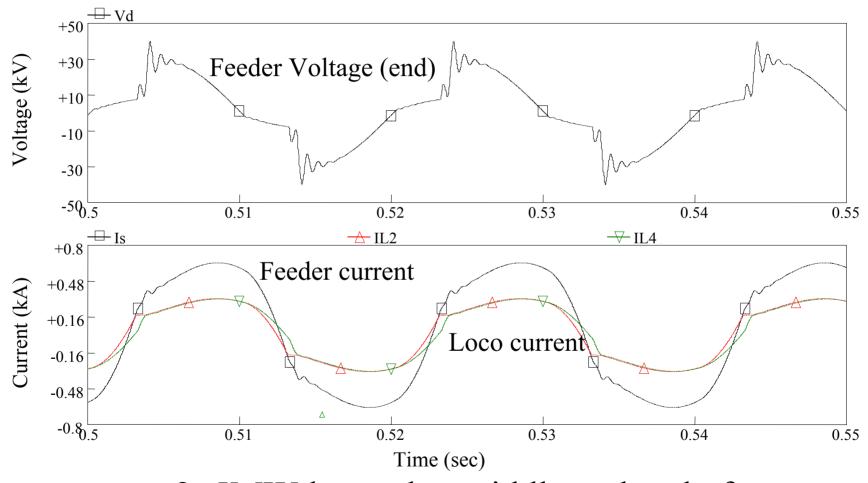


Active power filter control





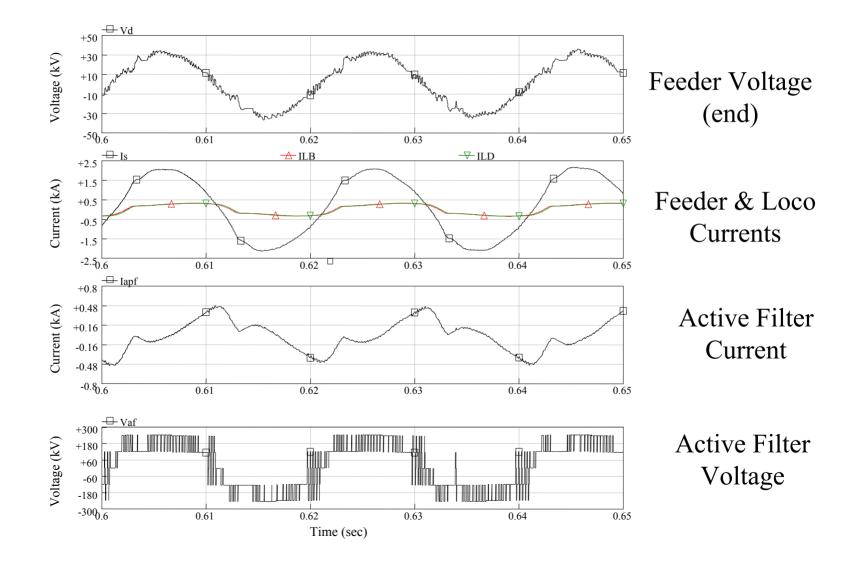
Simulation results Before compensation



2x5MW located at middle and end of feeder.

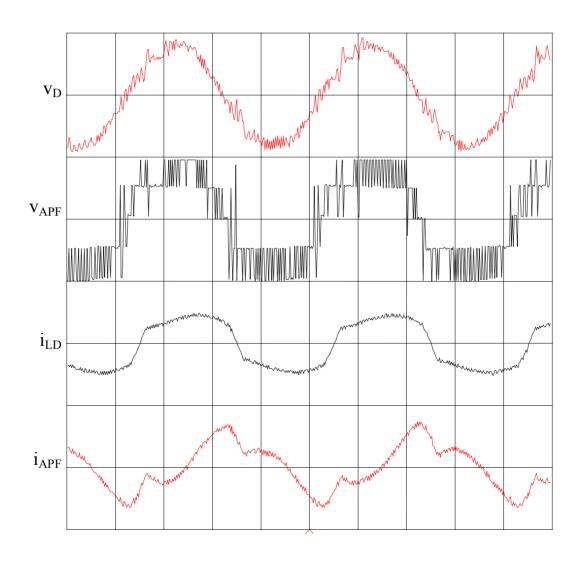


Simulation Results After compensation





Experimental results After compensation





Current Power Electronic Research Projects

- Distributed PE compensation systems for electrical grids
- Auxiliary power supplies for high voltage converters
- High performance drive systems
- EPLD implementation of high performance modulation
- Low inertia induction motor
- Intrinsically safe switch mode power supplies
- Reduction of EMI for power converter systems

What is the Future of Power Electronics?



Microelectronics



Moore's Law:
"Every 1.5 years
the cost of a 'bit'
drops 50%."

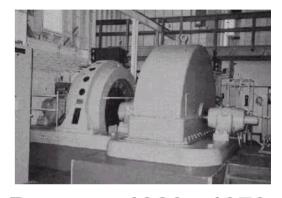


Power Electronics





Electric Power



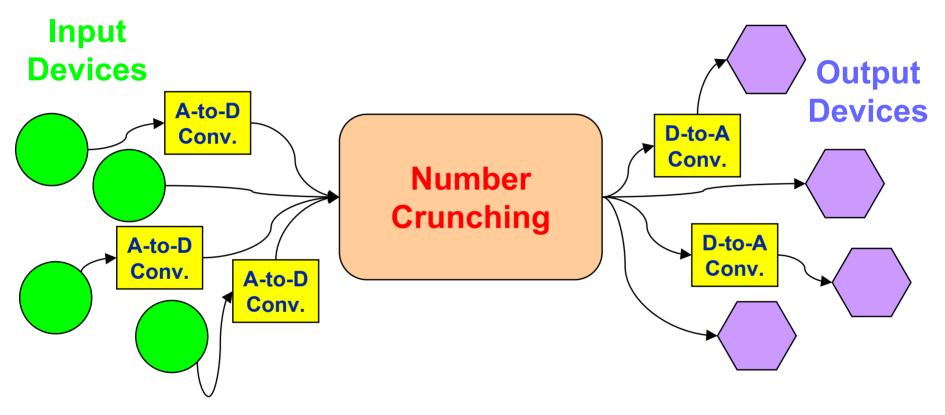
Between 1920 - 1970, every 1.5 years the cost of kWh dropped 5%.

Since then it is constant.





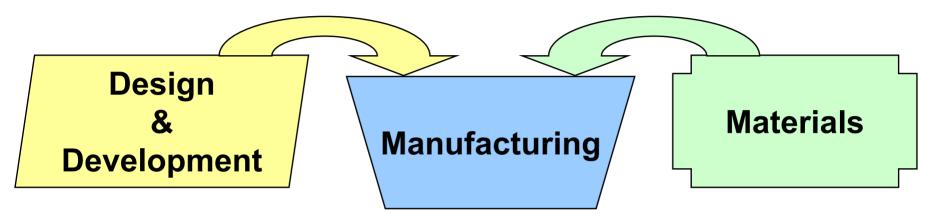
Digital Revolution



Most of Information Processing has been reduced to arithmetic and logic manipulation of binary numbers



Product Quality, Reliability, and Cost Factors:



- Optimized general purpose design
 - μP

- Automated dedicated design
 - **ASIC**

- Batch processing
 - Small number of steps
- Small number of different materials
- Efficient use of materials

Volume Production



Or Power Electronics Converter Design in the Last Century

Digital Controller

Digital Interface

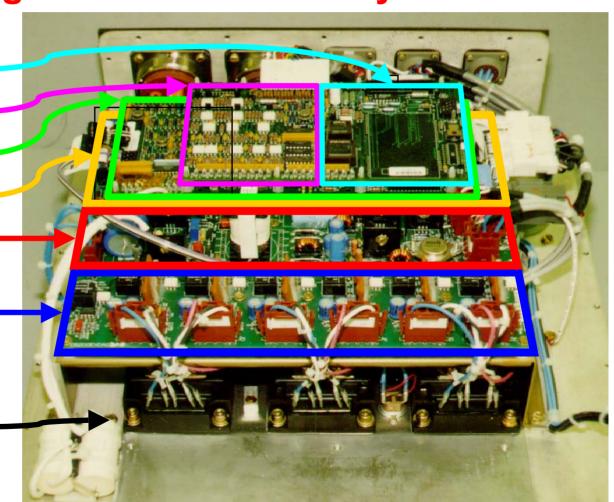
Analog Interface

Sensor Interface

Power Supplies

Gate Drives

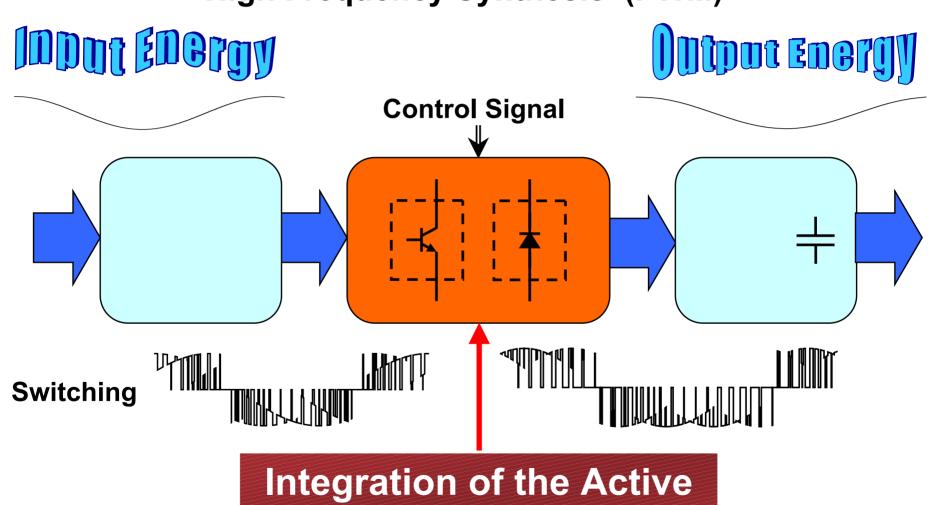
Power Stage







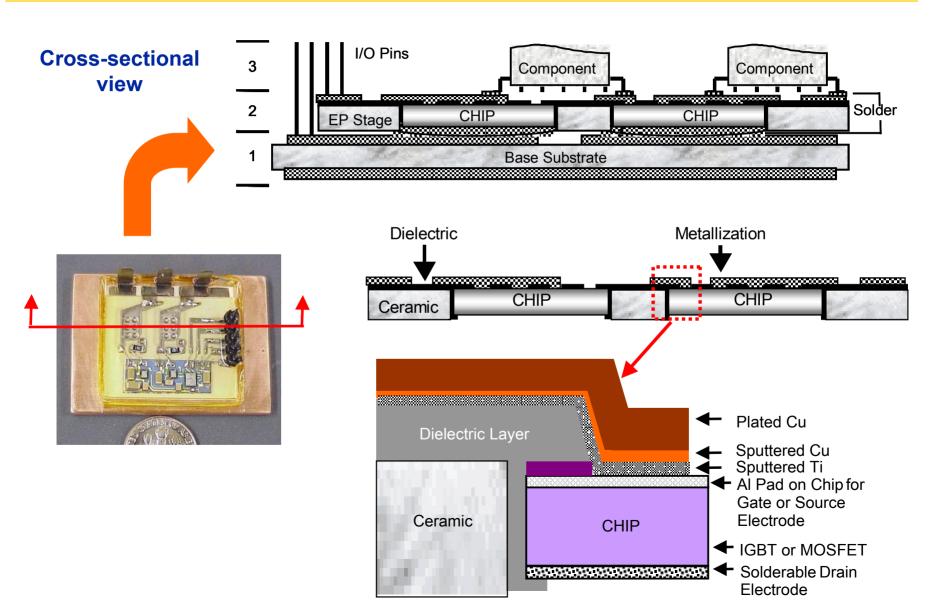
High Frequency Synthesis (PWM)



Integration of the Active Switching Stages

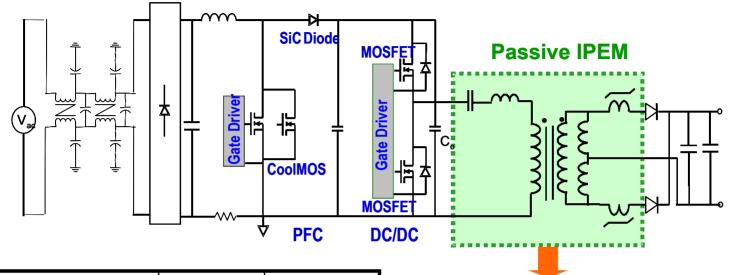


Active Switching Stages: Embedded Power

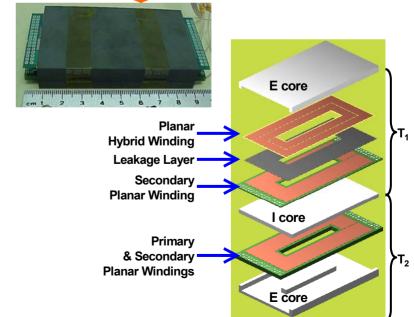




DPS Integration: Power Passives



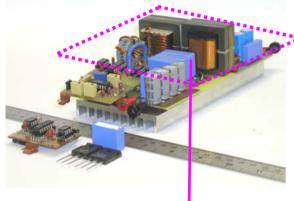
Parameter	Discrete	Passive IPEM	
Power (kVA)	1.0	1.0	
F _s (kHz)	45	45	
L _{m1,2} (uH)	45	45	
L _s (uH)	2	1.8	
C (uF)	2.3	2.5	
No. of Components	7	1	
No. of Terminals	17	5	
Total Profile (mm)	42	16	
Total Volume (cm ³)	168	82	
Power Density (W/in³)	97	200	

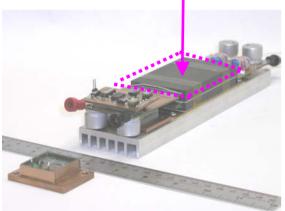


Improvements



Discrete DC/DC Converter

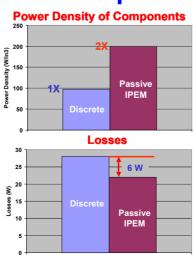


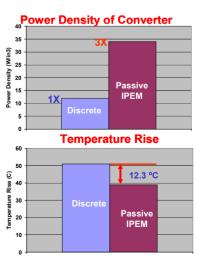


Integrated DC/DC Converter

Standard Fabrication techniques:

- · Direct metal deposition;
- Electro-plating;
- Photolithography;
- Wet-etching;
- Laser cutting;
- Reflow soldering;
- Improved power density, efficiency and thermal performance:





The Future





Pout

IECON 2013

Pin



- Electrical Power at Monash University a short walk through history
- What is this business called Power Electronics?
- Power Electronics research activities at Monash
- Other Electrical Power Research Activities
 - The EPRI Project
 - High Voltage
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- Summary





EPRI-Monash Work: Moisture in Transformers

- Started in mid 1990's to investigate aging transformer insulation
- One of the longest running EPRI funded projects in the world
- A world leader in modelling moisture content in electrical power transformers
- Headed by Dr Valery Davydov







Moisture in Thick Insulation: Electrical Treeing and Deterioration



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Moisture in Thin Insulation: Failure of the Transformer



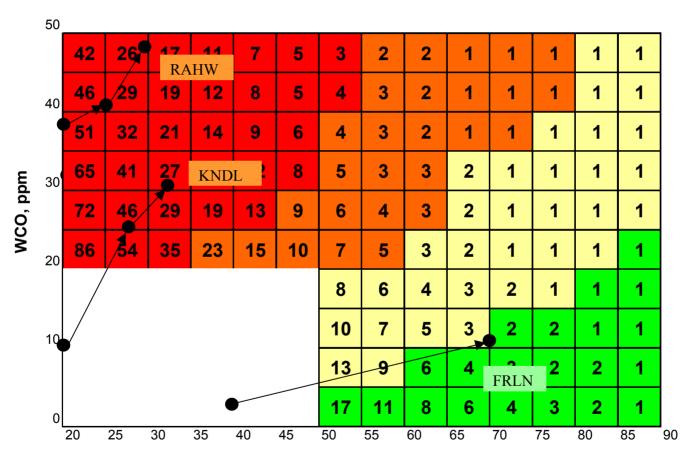


Moisture Determination Procedure

- 1. Measure water content of oil at low temperature, i.e. when oil temperature indicator reads minimum value for the day
- Measure water content of oil taken from the same port at higher temperature (can be on the same day, depending on oil temperature cycle)
- 3. Plot results of two consecutive measurements on the Color Chart
- 4. Observe where the rate of change in WCO vector is headed. Direction of this vector is indicative of moisture state in transformer
- 5. If both measurements fall into the uncertain area, repeat the measurements during the higher temperature season or during the load increase period

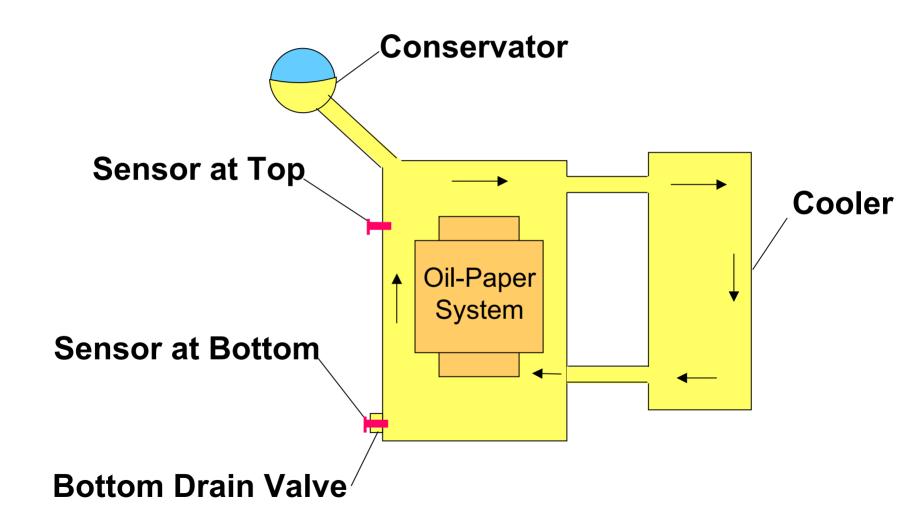


Classification Chart Usage



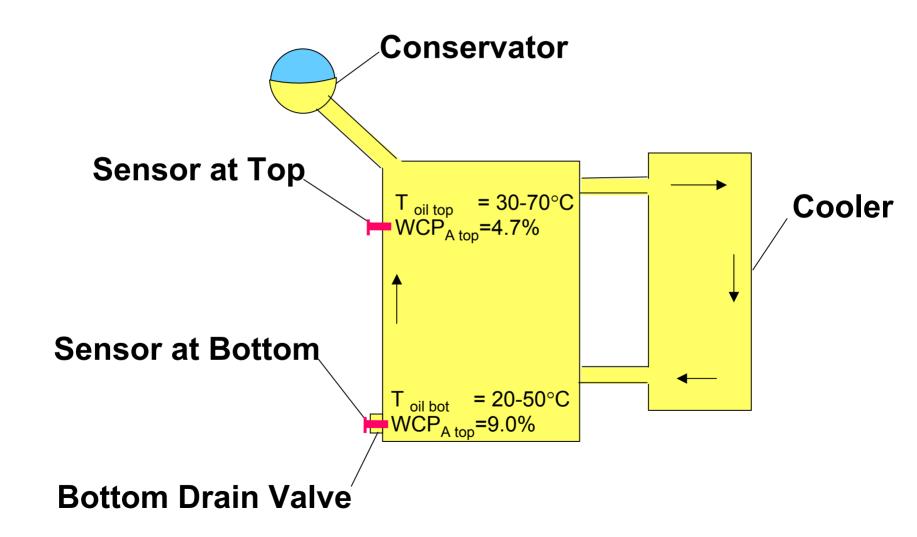


Trf with Natural Oil Circulation:Position of Sensors





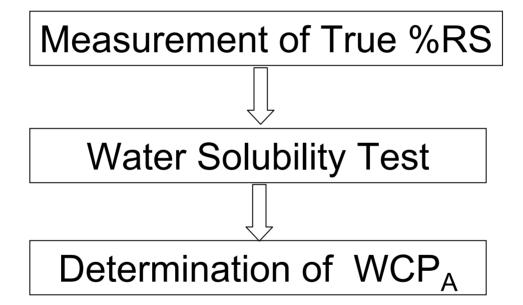
Results of Moisture Assessment





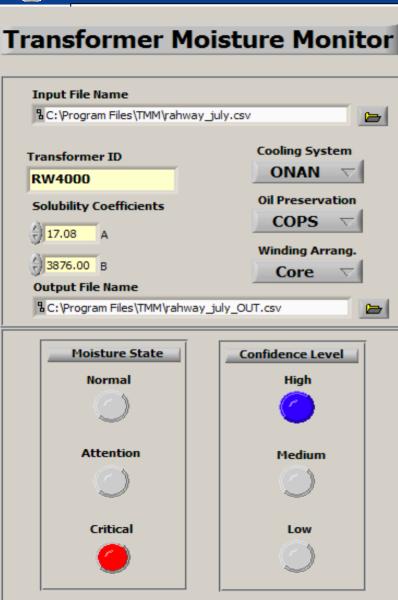


Monash WIP Algorithm (Simplified)



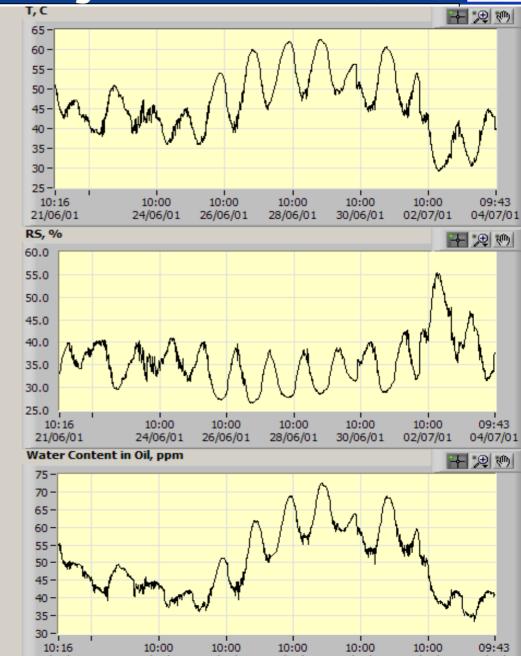
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CL 0.73

WCP, % 4.91





New Laboratory for the EPRI-Monash Project

- Monash University has invested a sum of approx. USD \$250,000 from its non-EPRI funds into construction of the New EPRI-Monash Project Laboratory
- Another USD \$50,000 from non-EPRI funds are being spent for purchasing laboratory equipment
- The New Lab will become fully operational following installation and commissioning of the new equipment in 2004



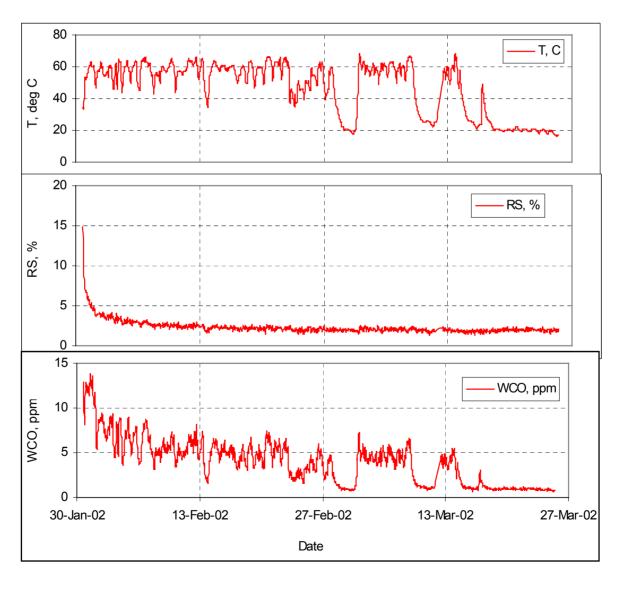
Monash Assessment of On-Load Dryout of EdF 22.5 MVA Trf

<u>Aims</u>

- Dry out the transformer on-load
- Assess dryout using Monash WIP algorithm
- Compare FRA signatures before and after to assess effect

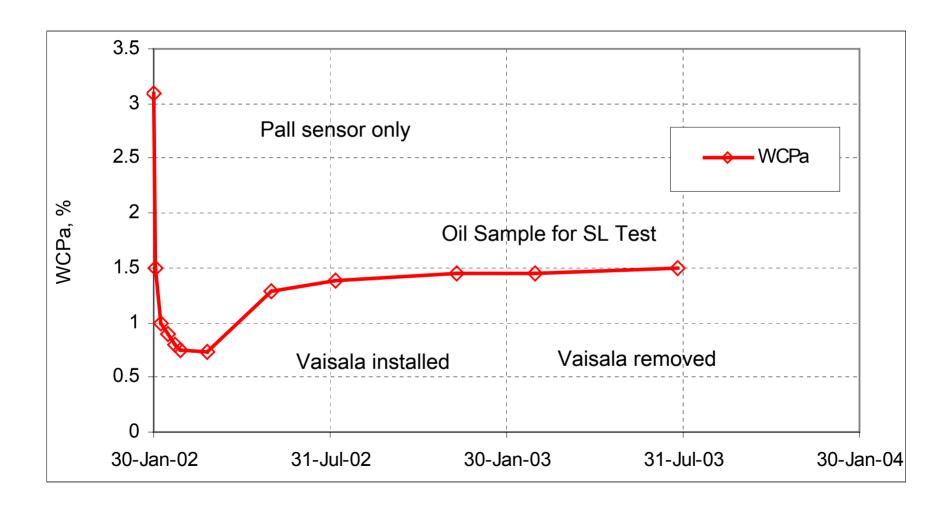


Monitoring of On-Load Drying for 8 Weeks



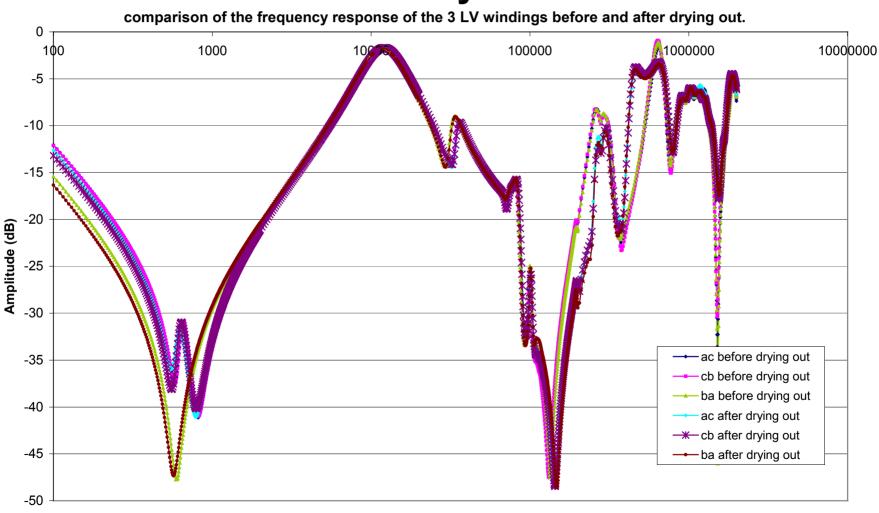


Changes in Active WCP during and after Dryout





FRA Signatures for EdF Transformer before and after Dryout





Factors which may affect FRA Signatures following Dryout

- Changes in the temperature of transformer
- Changes in moisture content of insulation
- Possible slackness of transformer windings due to reduction of

FRA Studies conducted in 2003

- Changes in the temperature of windings
- Changes in moisture content of insulation due to dryout
- Changes in geometry of windings due to a mechanical shift following re-clamping of the new transformer

Tests conducted on new transformer and on Monash model

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66 kV Winding of the WTC New 150 MVA, 220/66/11 kV Transformer





Proposed FRA Studies for 2004-06 (ARC Project)

- Effect of changes in clamping pressure simulated on test models
- Effect of winding slackness simulated on test models
- Effect of dryout of newly built and older repaired transformers at the plant
- Effect of on-load dryout in the field



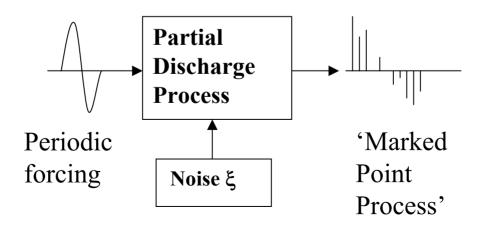


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PARTIAL DISCHARGE ANALYSIS A DETERMINISTIC APPROACH

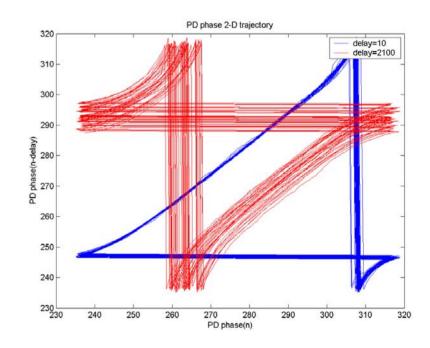
Input-output representation of partial discharge process





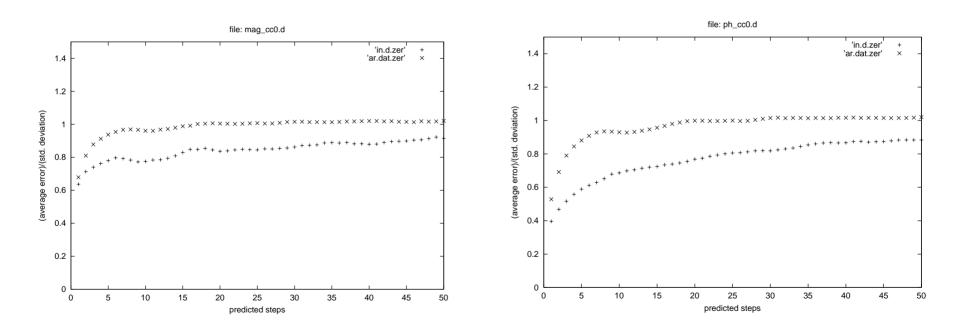
Deterministic dynamic model

$$PD_{ph}(n+1), PD_{m}(n+1) = f[PD_{ph}(n), PD_{m}(n), \cdots, PD_{ph}(1), PD_{m}(1)]$$



* 'Apparently stochastic' output from a deterministic process

Stochastic vs. non-linear – which one predicts better?

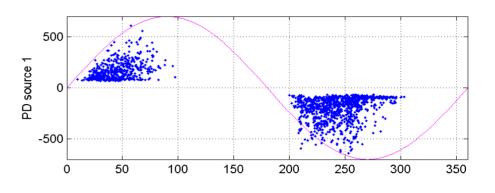


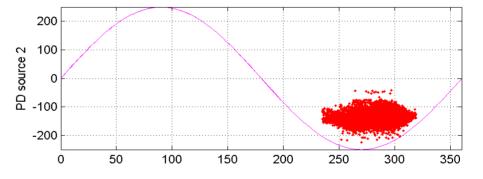
PD phase rounding grown Arc(10) model (XXX) and the local linear model (+++)

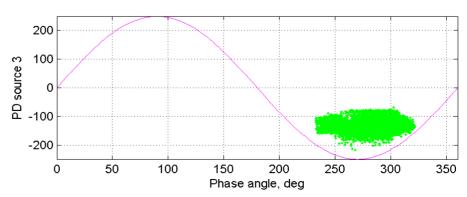


Classified PD signals

Phase resolved plots



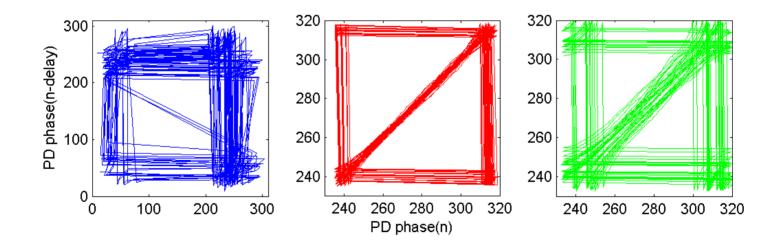






Classified PD signals

Trajectory plots





Classification results

Confusion table of RMS errors for classified series

		Reference series							
		A	В	С	D	Е	F	G	Н
Clas sifie d serie s	A: PD source 1	0.84	1.06	1.09	1.4	1.56	1.2	1.22	1.03
	B: PD source 2	1.12	0.52	0.73	1.74	1.35	1.06	1.13	1.06
	C: PD source 3	1.08	0.62	0.43	1.77	1.34	1.02	1.13	1.01
	D: PD simulated	1.05	1.26	1.22	0.04	1.1	1.08	1.39	1.15
	E: periodic	1.24	1.09	1.13	1.41	0.01	0.51	1.39	1.03
	F: periodic+noise	1.55	1.3	1.39	2.08	1.07	0.59	1.87	1.07
	G: chaotic cont.	1.11	1.04	0.98	1.59	1.49	1.15	0.09	1.01
	H: chaotic disc.	1.13	1.11	1.13	1.48	1.37	1.1	1.29	1.01



Is classification robust?

Confusion table of RMS errors for the robustness test

		Reference series					
		A	В	C	D	Е	F
Cla ssifi ed seri es	A: periodic, n/s=0	0.03	0.29	0.47	0.61	0.67	1.01
	B: periodic, n/s=20%	0.31	0.23	0.37	0.57	0.6	1.02
	C: periodic, n/s=40%	0.73	0.45	0.39	0.54	0.53	1.01
	D: periodic, n/s=60%	0.96	0.68	0.56	0.63	0.61	1.04
	E: periodic, n/s=80%	1.08	0.83	0.69	0.72	0.71	1.06
	F: random Gaussian	1.65	1.4	1.2	1.14	1.08	1.02

Classification seems robust for noise levels up to 50% of the signal



Signal discrimination by non-linear dynamics

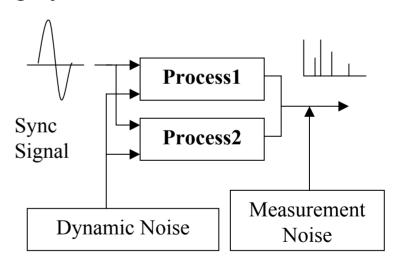
This idea is demonstrated by using synthetic data

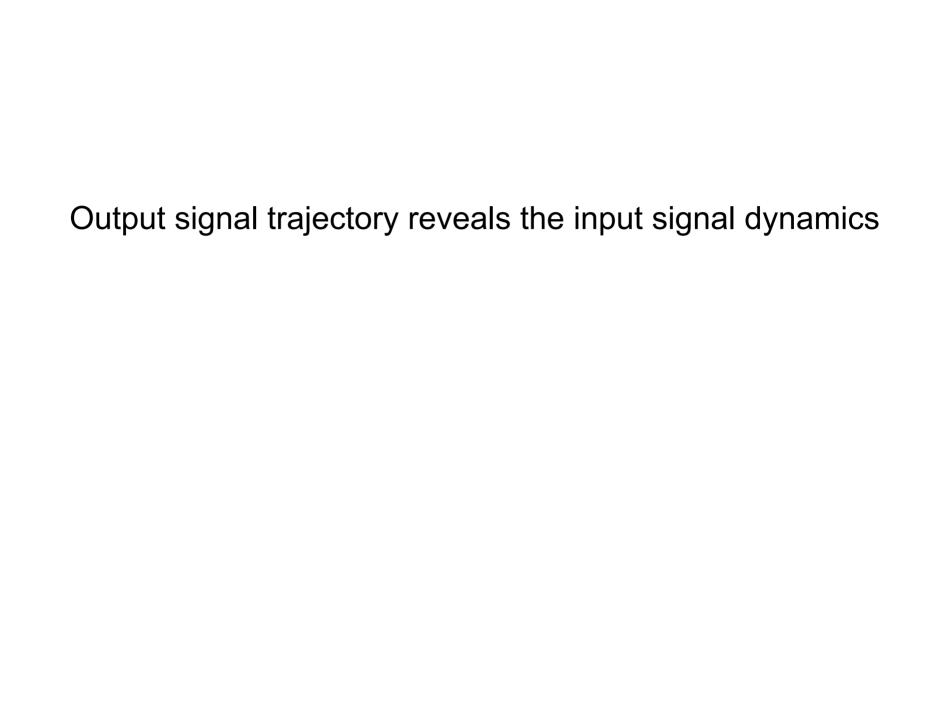
- Process 1
 Logistic generator (chaotic)
- Process 2

$$x_{n+1}=2\pi \cdot \sin(x_n)$$

Processes synchronised by external signal

Random noise added to both inputs and the output







Conclusions

- Deterministic model predicts better than the stochastic one, so PD process is likely to have dominating deterministic component
- The error of prediction can be used as the discriminating statistic for PD source identification
- Mixed signals can be unscrambled by using trajectory plots, a promise for discrimination of PDs from mixed sources



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Australia: Target 2% new renewables by 2010

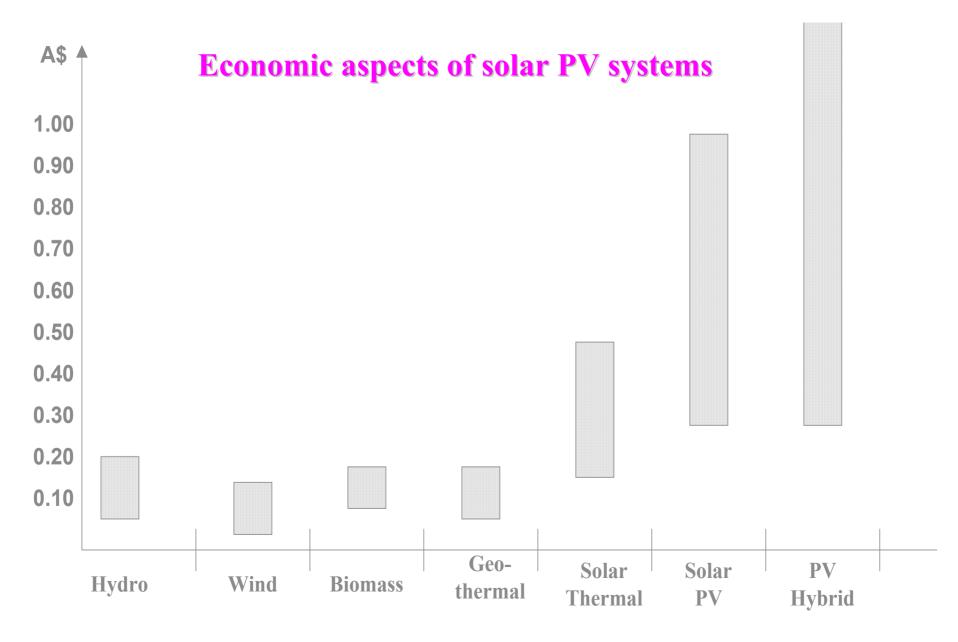
Solar Photovoltaic, Wind and Biomass

Main applications of solar PV energy systems

- Off-Grid Domestic
- Off-Grid Non-Domestic
- Mini Grid Hybrid
- Grid-tied distributed
- Grid-tied central

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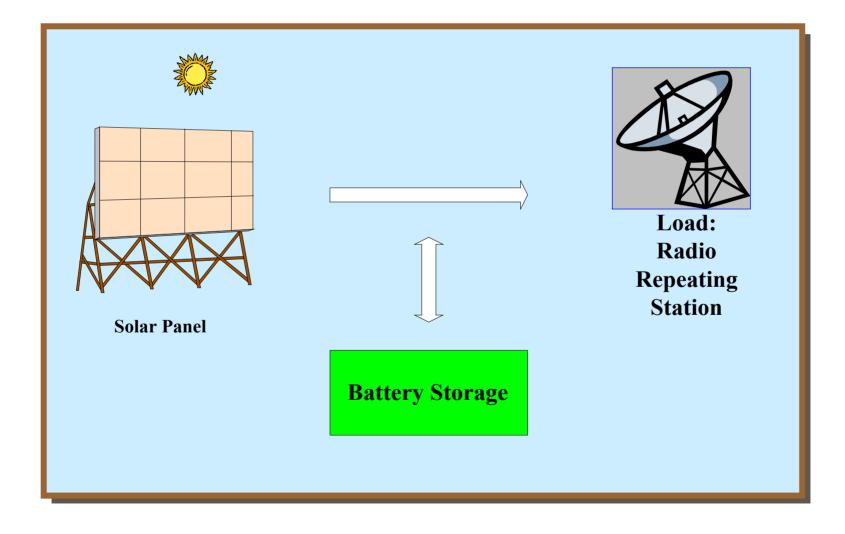




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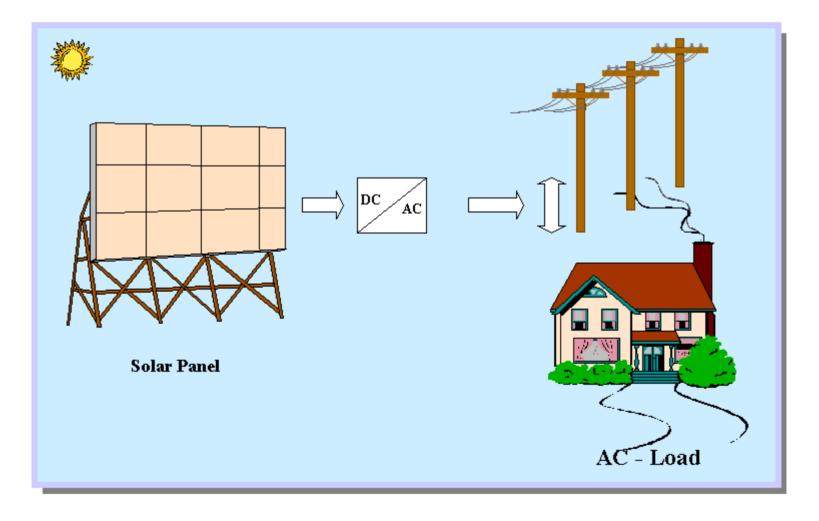
Design and Optimum sizing of PV systems for Telecommunication Companies, ie Telstra



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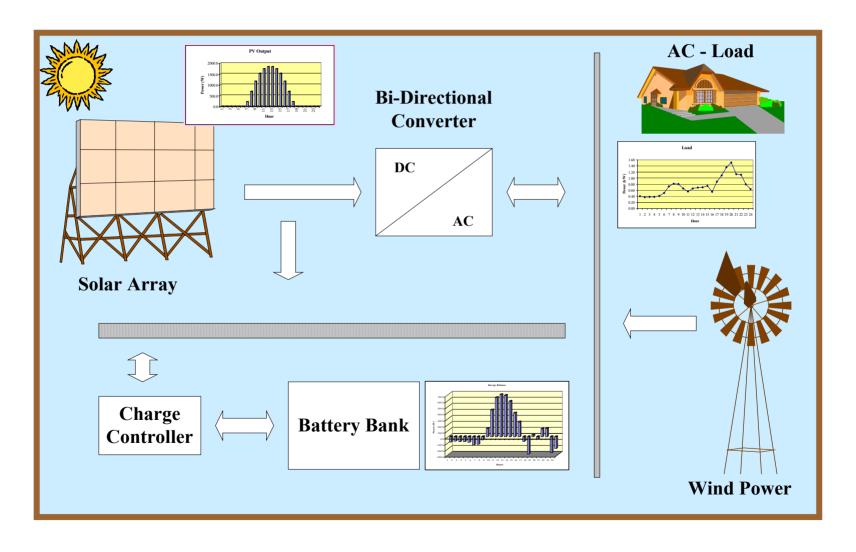
Grid-tied PV system, Quality of Electricity Islanding, Harmonics & Voltage variation



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Hybrid systems, Modelling, Performance prediction





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- Research Opportunities electrical energy conversion applications

(Centre for Energy and Power Electronics?)